

## Article

# Durability Studies of Solar Reflectors Used in Concentrating Solar Thermal Technologies under Corrosive Sulfurous Atmospheres

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**Abstract:** Concentrating solar thermal (CST) technologies are a feasible and promising option to tackle worldwide energy problems. These solar facilities are sometimes located near industrial sites, where their main components—including concentrating solar reflectors—are prone to significant degradation caused by corrosive agents, especially in the presence of sulfurous atmospheres such as H<sub>2</sub>S and SO<sub>2</sub>. This paper focuses on analyzing the influence of sulfurous atmospheres on the durability of reflector materials used in CST technologies. To this end, accelerated aging tests were performed on the most commonly used materials found in solar reflectors (i.e., thick silvered glass and aluminum-based reflectors) by applying the same concentrations of H<sub>2</sub>S and SO<sub>2</sub> under the same conditions of temperature and relative humidity. The results showed that the solar reflectors based on a silver reflective layer are significantly corroded by H<sub>2</sub>S atmospheres—several corrosion defects were found in the samples tested. However, those based on aluminum were barely affected by sulfurous environments in the conditions tested. Nonetheless, the study suggests that both reflector types are suitable candidates, depending on the purpose of the CST technology in question and the specific environmental conditions.

**Keywords:** renewable energy; concentrating solar thermal technology; solar reflector; durability; corrosive sulfurous atmosphere; industrial environment

## 1. Introduction

Concentrating solar thermal (CST) technologies are a feasible solution for worldwide energy problems. Currently, the power of CST plants installed and under operation around the world is 4.845 GW<sub>e</sub>—with 47.5% of this power generated in Spain [1]. This technology is not only a real player in the renewable energy mix, but also represents a truly promising option for the future. The International Energy Agency (IEA) forecasts in its 2014 technology roadmap that this technology will cover 11% of the total power generation by 2050 [2].

Concentrating solar collectors are sometimes located near industrial sites. This is not only in CST plants for power production, but also in solar facilities to feed industrial processes' heat demands [3]. In these cases, collectors are prone to corrosion, especially in the presence of sulfurous atmospheres, such as hydrogen sulfide (H<sub>2</sub>S) and sulfur dioxide (SO<sub>2</sub>). Reflectors are a vital part of these facilities and must comply with several requirements, including high performance for extended periods of time,

even in aggressive environments [4]. When these solar facilities are exposed to these corrosive gases, the metallic components of solar reflectors are highly susceptible to degradation. The components are mainly silver and copper in the case of second-surface silvered-glass reflectors, and aluminum in the case of first-surface aluminum reflectors.

Hydrogen sulfide is one of the reduced sulfur gaseous forms present at different industrial sites, along with carbonyl sulfide, sulfur vapor, and mercaptans. The main producers of  $H_2S$  are rubber manufactures, sewage and waste-water treatment plants, petroleum refineries, coal-generation power plants, and pulp and paper mills [5,6]. Other sources that contribute to  $H_2S$  emission are farms [7], marshes, and volcanoes [8], with  $H_2S$  resulting from both anthropogenic activity and natural origins.  $SO_2$  is one of the most abundant atmospheric contaminants, and is mainly emitted in the combustion of sulfur-containing fossil fuels and the smelting of metal sulfide ores [7,9]. The International Electrotechnical Commission (IEC) has established limits for different polluted environments on the concentration values of  $H_2S$  and  $SO_2$ , as illustrated in Table 1 [10]. As shown in this table,  $SO_2$  levels are consistently higher than  $H_2S$  with the exception of the environment inside industries. However, this also depends on the industry type.

**Table 1.** IEC classifications of different polluted environments by their  $H_2S$  and  $SO_2$  concentrations (values in ppm).

Pollutant	Clean Room	Controlled Environment	Rural /Urban	Heavy Urban or Industries	Adjacent to Industries	Inside Industries
$H_2S$	0.001	0.004	0.004	0.2	4.1	28.5
$SO_2$	0.038	0.038	0.038	0.4	3.8	15.3

The existing research on the durability of solar components carried out in the past five years have predominantly been devoted to studying erosive events [11–14] and saline environments [15,16], as CST plants are frequently located in desert environments and/or near coastal sites. Accordingly, extensive outdoor campaigns have taken place to gain more knowledge of the atmospheric corrosion of metals and solar reflectors [17,18]. Modeling and service lifetime prediction studies on new solar reflector candidates have also taken place [19,20].

Unfortunately, few studies have approached the durability issues of solar reflector materials exposed to polluted atmospheres [4]. This new field of study requires specific testing conditions and evaluation of materials that are wholly different from those previously used. Recently, the significant development of small-sized CST collectors used to supply heat to industrial processes has given way to new research needs. Therefore, the focus of research related to the durability of solar reflectors must be redirected to include industrial environments exposed to corrosive gases. One research area that must be approached is the analysis of the influence of sulfurous atmospheres on the durability of reflector materials used in CST technologies.

To date, the few research studies conducted on this specific topic are devoted to the effects of humid sulfur-containing atmospheres [21,22], in addition to the studies already carried out by the authors' research group with  $H_2S$  [23] and acid rain [24,25]. These differ from the present study in that the effect of each gas was assessed independently without comparing it to the effects of other gases. However, examples of active research on the effects of this type of environments on the pure metals present in solar reflectors can be found in the literature [26–29]. Some of the conclusions derived from these studies may also be of use for the solar collectors of the present study.

The aim of this study is to compare the effects of two sulfurous gases ( $H_2S$  and  $SO_2$ ) on solar reflector materials, when performing accelerated aging tests under the same conditions of gas concentration, temperature ( $T$ ) and relative humidity ( $RH$ ). Unlike previous studies, this study carries out a comparative analysis of the effects of two sulfurous gases on reflector performance. In addition, this study provides recommendations about which reflector type is more appropriate for a specific polluted environment. The main conclusions drawn are that the reflective silver layer is

easily corroded by H<sub>2</sub>S atmospheres, especially in pre-damaged zones, while the reflective layer of aluminum is barely affected by SO<sub>2</sub> or H<sub>2</sub>S under the testing conditions. Synergism with other factors such as *T* and *RH* were considered significant accelerating agents in the corrosion process of solar reflector materials.

## 2. Materials and Methods

This section describes the solar reflector materials tested in this work, the testing approach followed, and the methods used to evaluate the results obtained. First, the experimental approach is described.

### 2.1. Experimental Approach

Reflector material samples were prepared and extracted from bigger facets in a format suitable for testing and assessment (see Section 2.2). They were rinsed with deionized water before their initial characterization, which mainly consisted of reflectance measurements and optical microscope (OM) inspections (see Section 2.4). After the initial assessment, the samples were tested in accelerated aging chambers, as described in Section 2.3. The two reflector types were weathered at the same time and under the same *T* and *RH* conditions, only modifying the corrosive gas (H<sub>2</sub>S, SO<sub>2</sub> or without gas) between tests. The potential effects of the testing atmospheres were evaluated at different points of the tests, as explained in Section 2.3 with the analytical instrumentation described in Section 2.4.

### 2.2. Description of Materials

Two different reflector samples were studied for this article due to their widespread use in CST facilities [4]. Both second-surface silvered glass reflectors with one originally protected edge and first-surface aluminum reflectors were analyzed to assess their behavior when exposed to two corrosive gases, namely SO<sub>2</sub> and H<sub>2</sub>S. Aluminum reflector samples had measurements of 12 × 12 cm<sup>2</sup> and silvered glass reflectors measured 10 × 10 cm<sup>2</sup>. Both the sizes were appropriate to test the samples inside the chambers and to measure them in the evaluation equipment. Three samples per reflector type were used to obtain statistically representative data.

The second-surface silvered reflector samples were cut out of a commercial parabolic-trough facet, boasting three cut or unprotected edges and one originally protected edge. In the protected edge, the reflective layer was totally covered by several paint layers. In principle, this would make the edge more effective against external agents, including corrosive gases. Conversely, the remaining three cut edges were completely exposed to the corrosive environment and were significantly more vulnerable to weathering effects. An additional initial damage was deliberately performed in order to expose the reflector layer directly to the corrosive atmosphere. This damage was performed with a normalized scratching tool model 426 90064/009 manufactured by Erichsen [30], resulting in a 2 cm-long scratch on the back painted side of the samples. This pre-damaged reflector area attempted to simulate the corrosion experienced by samples that may face sandstorm conditions [14], inappropriate manipulation, aggressive cleaning procedures [31], etc.

Regarding the first-surface aluminum samples, the same scratch procedure was carried out on the reflectors' front surface to evaluate the corrosion acceleration caused by this pre-damage. However, this material does not have protected edges as commercial aluminum facets are not manufactured with this type of edge protection.

### 2.3. Experimental Campaign

Two different test chambers were used to perform the experiments—one filled with corrosive gas and one without. Both chambers could be controlled in remote mode. Additionally, the chambers were equipped with *T* and *RH* sensors, which could not only control the atmospheric conditions during the test, but also switch off the device, should a problem have occurred. As a security measure, several gas detectors were installed inside the room where the chambers were placed in the event of a gas leakage.

An SC 340 MH weathering chamber with a testing volume of 340 l and manufactured by Atlas was used for the tests without corrosive gases (Figure 1a). The chamber could combine  $T$ ,  $RH$  and irradiation, with an operating  $T$  range of 10–90 °C, and a  $RH$  range of 10–90%.

A VCC<sup>3</sup> 0034 Vötsch chamber with a testing capacity of 335 l was used to test the samples in the environments with the two gases under study (Figure 1b). The operating  $T$  range of this chamber was 15–60 °C, and the maximum  $RH$  range is 10–85%. The chamber also had four different gas feed lines that allowed for single- and multiple-gas testing. The maximum permissible gas concentrations inside the chamber were 25 ppm for H<sub>2</sub>S, SO<sub>2</sub> and NO<sub>2</sub>, and 1 ppm for Cl<sub>2</sub>. For this study, two of the most aggressive gases found in industrial atmospheres (SO<sub>2</sub> and H<sub>2</sub>S) were tested independently. In both cases, the carrier gas flow (SO<sub>2</sub> and H<sub>2</sub>S diluted in N<sub>2</sub>) was driven through an absorbance column with a specific desiccant and a particle filter to remove impurities before entering the chamber.



**Figure 1.** Weathering chambers used in the corrosive tests: (a) SC 340 MH; (b) VCC<sup>3</sup> 0034 Vötsch.

The experimental campaign with corrosive gases was based on the international standard IEC 60068-2-43:2003, environmental testing—Part 2-43: Test Kd: Hydrogen sulphide test for contacts and connections [32]. This standard was originally conceived to study the influence of H<sub>2</sub>S environments in silver alloys and coatings. However, IEC parameters were modified for this study to reach the maximum operating  $T$  and  $RH$  of the weathering chamber.

Three different experiments were performed at the same  $T$  and  $RH$  (that is,  $T$  = 60 °C and  $RH$  = 85%). The only variation was the gas added. The first test was carried out without sulfurous gas, i.e.,  $T$  and  $RH$  were the only parameters involved in the test. The other two tests were carried out in the presence of the two gases under analysis (SO<sub>2</sub> and H<sub>2</sub>S)—both with a concentration of 15 ppm. These extreme conditions are rarely found in other studies. There may have been synergistic degradation mechanisms between the different parameters, especially in the tests with gas.

All the samples were placed on an inert-material tray at a 45° tilt angle inside the weathering chambers. The samples were taken out to be meticulously analyzed at regular intervals. These were on days 4, 7, 10, 14 and 21. Before being characterized, samples were rinsed with deionized water to remove any dirt or corrosion products on the reflector surface.

#### 2.4. Description of Instruments

To determine and quantify the degradation of the solar reflectors caused by corrosive atmospheres, the following analytical instrumentation was used:

- A portable reflectometer model 15R-USB manufactured by Devices and Services [33] was used to calculate the monochromatic specular reflectance,  $\rho_{\lambda,\phi}$ , in a wavelength range of 635–685 nm with

a peak at 660 nm,  $\rho_{\lambda,\varphi}$  (660 nm, 15°, 12.5 mrad). An acceptance angle of 12.5 mrad was used to measure nine different areas of the reflector sample, as illustrated in Figure 2. This image shows that the scratch is exactly on the square A8. Hence,  $\rho_{\lambda,\varphi}$  is expected to be lower in this pre-damaged area than in the rest of the sample and therefore was treated independently. Three measurements on the square A8 were taken to provide statistics on the results. The remaining eight areas were considered consistent and as a result their reflectance average represents the reflectance value of the undamaged surface.

- Solar-weighted hemispherical reflectance,  $\rho_{s,h}$ , was measured with a spectrophotometer model Lambda 1050 with a 150 mm diameter integrating-sphere accessory manufactured by Perkin Elmer [34]. The wavelength range measured was 280–2500 nm with an incidence angle of 8°,  $\rho_{s,h}$  ([280, 2500] nm, 8°, h). This parameter was calculated according to the ISO Standard 9050 formulation [35] using the solar direct radiation spectrum from ASTM G173-03 [36]. The samples were measured at the central position (A5 zone in Figure 2) by rotating them three times to check for any possible anisotropy.
- A 3D OM model Axio CSM 700 manufactured by Zeiss was used to follow the evolution of prospective defects [37]. Pictures of the defects, such as spots or edge corrosion, were taken at 10× magnification to assess the corrosion originated in the reflector layer. Pictures of the reflectors surfaces were taken every time the analysis was carried out.

A1	A4	A7
A2	A5	A8
A3	A6	A9

**Figure 2.** Selected square areas for  $\rho_{\lambda,\varphi}$  measurements on the reflectors samples. The scratch is in square A8, while the other areas correspond to the initially undamaged reflective surface.

### 3. Results

This section sets out the results obtained in two different reflector types (second-surface silvered glass and first-surface aluminum) subjected to extreme conditions of  $T$  and  $RH$  and two corrosive gases typically found in industrial environments— $\text{SO}_2$  and  $\text{H}_2\text{S}$ . An additional test performed under the same  $T$  and  $RH$  testing conditions but without sulfurous gases was carried out to verify if the potential deterioration of the materials was indeed caused by the presence of the corrosive gases. Several reflectance parameters, such as the monochromatic specular reflectance,  $\rho_{\lambda,\varphi}$ , and the solar-weighted hemispherical reflectance,  $\rho_{s,h}$ , were monitored in order to track the performance of the reflectors. Additionally, corrosion spots and the area of the scratch were carefully inspected with OM.

All the reflectance values were normalized to the initial values to properly compare the results and analyze the influence of the testing conditions on the two reflector types. The initial reflectance values of the two reflector types are significantly different as shown in Table 2, with the silvered glass reflector having the best optical performance.

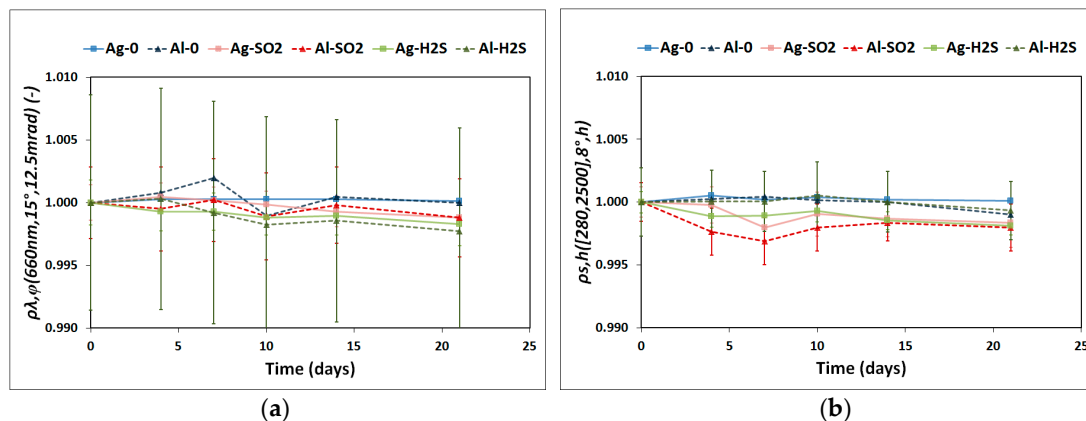
Figure 3 illustrates the results of the normalized  $\rho_{\lambda,\varphi}$  (a) and  $\rho_{s,h}$  (b) measured in the undamaged area of the reflector samples for the two reflectors and the three testing conditions. As can be seen in this figure, silvered glass reflectors are more degraded by  $\text{H}_2\text{S}$  than by  $\text{SO}_2$ , although the final values are very close. It also shows that in the test without gas, the material did not degrade. Concerning aluminum reflectors, there is a very subtle difference in the  $\rho_{s,h}$  results (Figure 3b), indicating a slightly



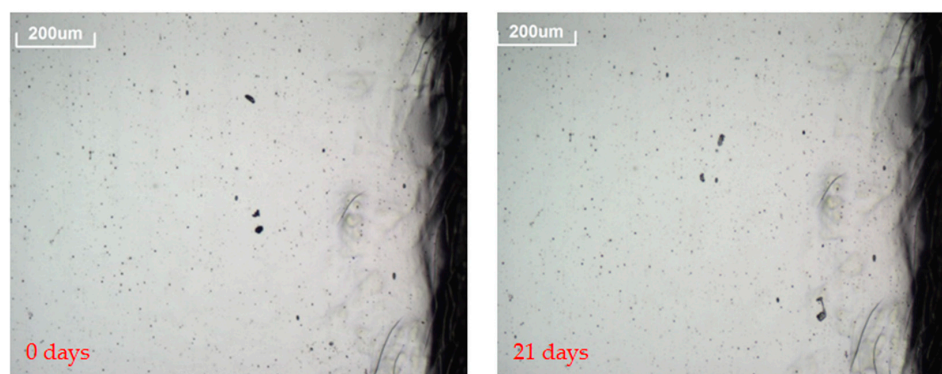
poorer behavior of this reflector type, when exposed to  $\text{SO}_2$  in comparison to  $\text{H}_2\text{S}$ . This difference cannot be confirmed with the  $\rho_{\lambda,\varphi}$  values (Figure 3a), as the uncertainty of the measurements is substantial. This is due to the inherent heterogeneity of this material as depicted by the standard deviations. This fact is corroborated by OM inspections, where there are no signs of corrosion developments, either on the cut edges or on the reflective surface of aluminum reflectors (see Figure 4).

**Table 2.** Initial reflectance values of the undamaged areas of the two reflector types under study.

Reflector Type	$\rho_{\lambda,\varphi}$ (660 nm, $15^\circ$ , 12.5 mrad)	$\rho_{s,h}$ ([280, 2500] nm, $8^\circ$ , h)
Silvered glass	$0.952 \pm 0.005$	$0.938 \pm 0.006$
Aluminum	$0.827 \pm 0.009$	$0.898 \pm 0.002$



**Figure 3.** Evolution of the normalized reflectance change on the areas not initially damaged for the tests throughout the 21 days of the experiments, both for silvered glass and aluminum reflectors: (a) Monochromatic specular reflectance; (b) Solar-weighted hemispherical reflectance (light-blue squares in the test without gas (Ag-0), light-red squares in the  $\text{SO}_2$  test (Ag- $\text{SO}_2$ ) and light-green squares for silvered glass reflectors in the  $\text{H}_2\text{S}$  test (Ag- $\text{H}_2\text{S}$ ) respectively; dark-blue in the test without gas (Al-0), dark-red in the  $\text{SO}_2$  test (Al- $\text{SO}_2$ ) and dark-green triangles for aluminum reflectors in the  $\text{H}_2\text{S}$  test (Al- $\text{H}_2\text{S}$ ), respectively).



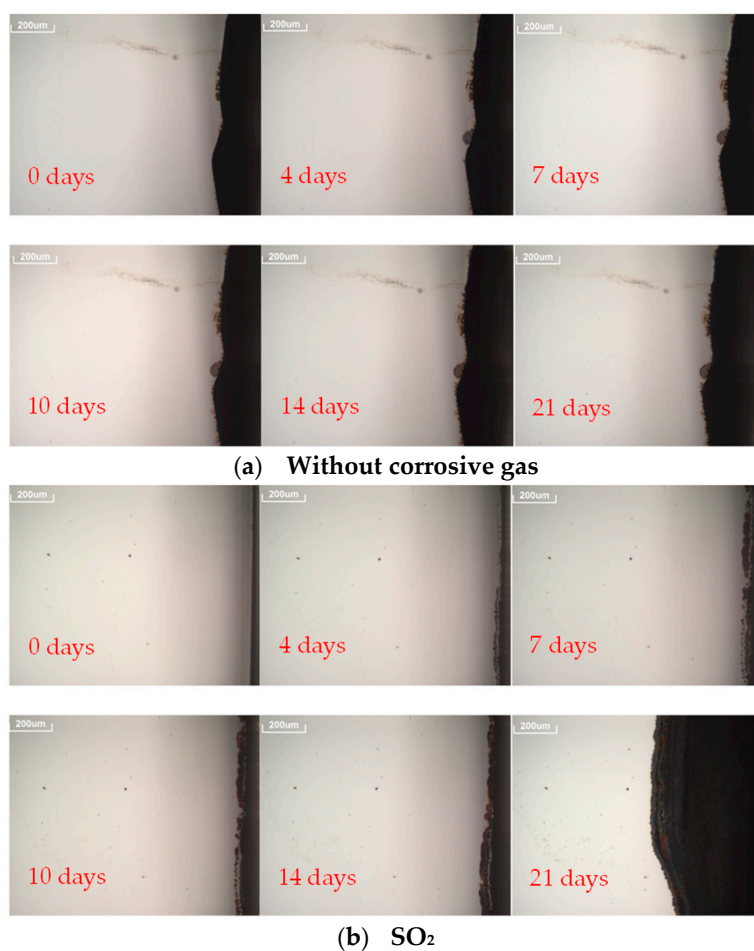
**Figure 4.** OM pictures of the cut edges and the reflective layer of aluminum reflectors in their initial state (0 days) and after 21 days of the  $\text{SO}_2$  test.

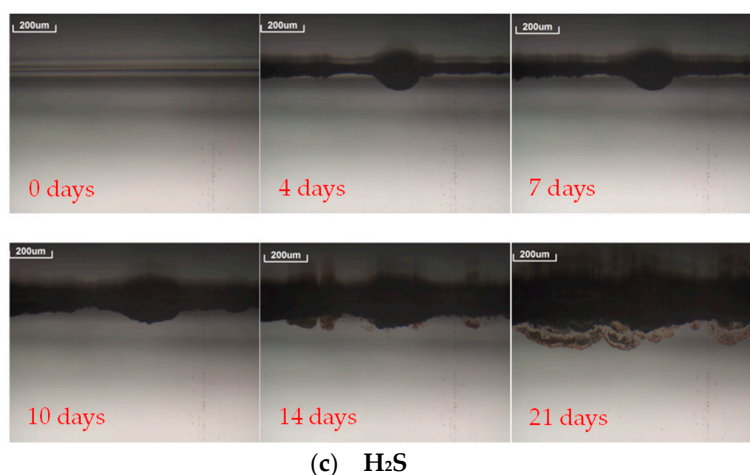
To verify the source of the reflectance reductions detected in the silvered glass reflectors, samples were also analyzed in depth with OM inspections after a certain period of testing time had elapsed (0, 4, 7, 10, 14 and 21 days). Table 3 summarizes the quantitative results obtained through OM analysis after testing the two reflector types for 21 days.

**Table 3.** Summary of the corrosion defects found with OM after testing silvered glass and aluminum reflectors for 21 days.

Type of Reflector	Type of Experiment	Undamaged Area		Pre-damaged Area	
		Mean Number of Spots	Maximum Corrosion Penetration in the Protected Edges ( $\mu\text{m}$ )	Maximum Corrosion Penetration in the Cut Edges ( $\mu\text{m}$ )	Increase of Scratch Width ( $\mu\text{m}$ )
Aluminum	Without Corrosive Gas	0	Only cut edges present in the samples	0	0
	SO <sub>2</sub>	0	Only cut edges present in the samples	0	0
	H <sub>2</sub> S	0	Only cut edges present in the samples	0	0
Silver	Without Corrosive Gas	0	0	209	45
	SO <sub>2</sub>	2	0	327	121
	H <sub>2</sub> S	24	564	685	901

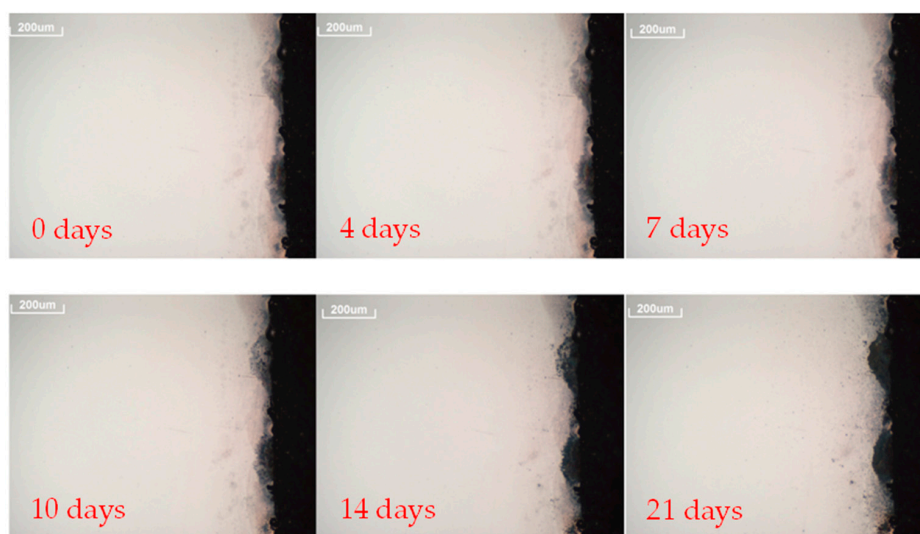
Figure 5 shows the evolution of the corrosion near the cut edges of silvered glass reflectors during the three tests performed. As depicted in both Figure 5 and Table 3, the corrosion caused by the tests with gases (b, c) under same  $T$  and  $RH$  conditions is considerably more aggressive than the one caused without corrosive gas (a)—with H<sub>2</sub>S (c) being the most harmful gaseous agent for this type of reflector.

**Figure 5.** Cont.



**Figure 5.** OM pictures of the evolution of corrosion in the cut edges after carrying out tests on silvered glass samples for 21 days: (a) Ag-0 test; (b) Ag-SO<sub>2</sub> test; (c) Ag-H<sub>2</sub>S test.

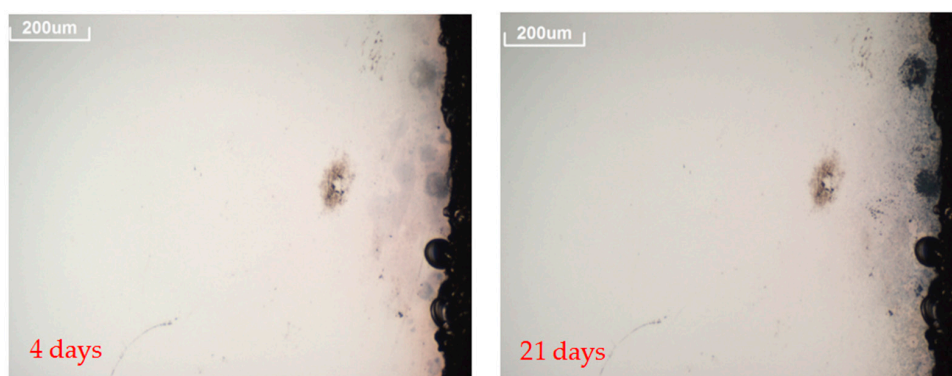
It is also noteworthy that during the H<sub>2</sub>S test performed on the silvered glass reflectors the protected edge was also significantly affected (see Figure 6 and Table 3), while in every other test the protected edges were not damaged.



**Figure 6.** OM pictures showing the evolution of the protected edges after performing the H<sub>2</sub>S test on the silvered glass samples for 21 days.

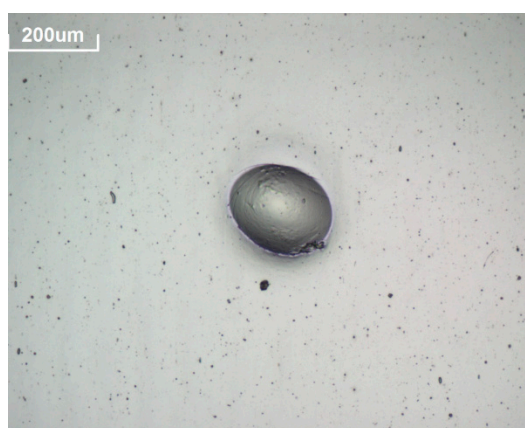
As shown in these images (Figures 5 and 6), corrosion appears gradually on the silver layer, attaining maximum development after 21 days. Localized corrosion spots on the silver layer were observed in both the H<sub>2</sub>S and SO<sub>2</sub> test. The number of spots was considerably higher when the experiment was performed in an H<sub>2</sub>S atmosphere (see Table 3). Typical spots near a protected edge can be seen in Figure 7, after 4 days and 21 days of the H<sub>2</sub>S test.





**Figure 7.** Evolution of microscopic spots near a protected edge in silvered glass reflectors of the H<sub>2</sub>S test after 4 days and 21 days.

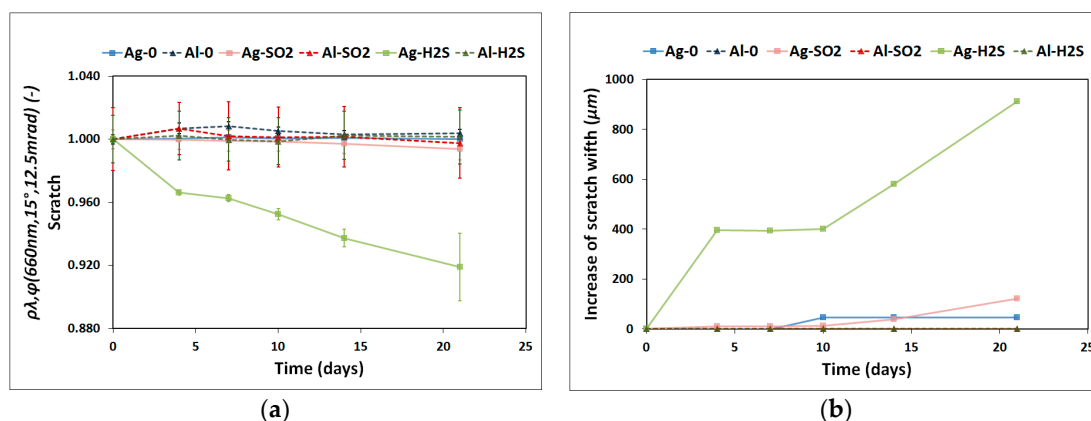
Aluminum reflectors did not suffer significant deterioration in either of the tests (see Table 3), but some degradation phenomena were observed after the SO<sub>2</sub> test, such as a few defects in the protective coating layer (illustrated in Figure 8).



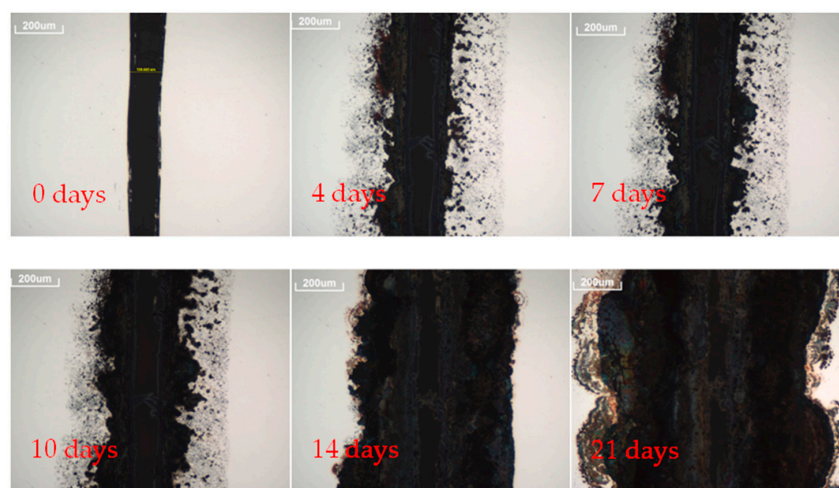
**Figure 8.** Microscopic defect found in the protective coating layer of an aluminum reflector after 21 days of the SO<sub>2</sub> test.

As mentioned in the methodology, studying the aggressiveness of the corrosive gases when a scratch is present on the reflector surface is of special interest as this often occurs through inappropriate manipulation of the mirror during mounting or manufacturing. To this effect, the normalized reflectance graph can be plotted to observe the evolution of scratch corrosion without being influenced by the initial scratch state. A graphic evolution of the scratch reflectance over 21 days can be seen in Figure 9a. A drastic decrease in  $\rho_{\lambda, \varphi}$  is observed on the scratch surface of the silvered reflector when the experiment is performed in an H<sub>2</sub>S atmosphere (up to 0.08 points), while no significant  $\rho_{\lambda, \varphi}$  decrease is detected under the other testing conditions. Similarly, there is an increase in scratch width caused by the development of corrosion, reaching a maximum value of 901 µm after 21 days of the H<sub>2</sub>S test (Figure 9b). Additionally, there is a slight increase in scratch width after the tests with SO<sub>2</sub> and without gas (121 and 45 µm, respectively). Regarding aluminum reflectors, no significant degradation is observed in either of the tests. This is in line with the previously reported results for the undamaged area of this type of reflectors.

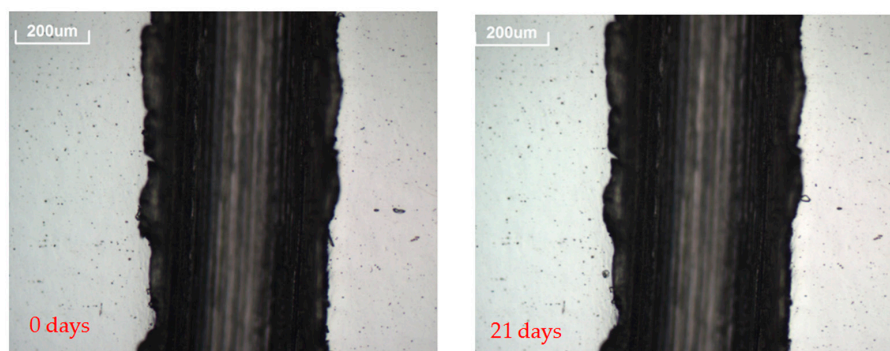
As shown in Figure 10, the deterioration of the scratch on the silvered glass samples during the H<sub>2</sub>S test can also be clearly observed in the OM pictures. However, Figure 11 shows no change in the scratch on aluminum reflectors after performing the SO<sub>2</sub> test for 21 days.



**Figure 9.** Evolution of the normalized reflectance change and increase in scratch width on the initially damaged areas of silvered glass and aluminum reflectors throughout 21 days of tests: (a) Normalized evolution of the change in monochromatic specular reflectance; (b) Increase of the maximum scratch width (light-blue squares in the test without gas (Ag-0), light-red squares in the SO<sub>2</sub> test (Ag-SO<sub>2</sub>) and light-green squares for silvered glass reflectors in the H<sub>2</sub>S test (Ag-H<sub>2</sub>S), respectively; dark-blue in the test without gas (Al-0), dark-red in the SO<sub>2</sub> test (Al-SO<sub>2</sub>), and dark-green triangles for aluminum reflectors and in the H<sub>2</sub>S test (Al-H<sub>2</sub>S), respectively).



**Figure 10.** OM pictures showing the evolution of the scratch on the reflective side of silvered glass reflectors after performing the H<sub>2</sub>S test for 21 days.



**Figure 11.** OM pictures of the scratch on aluminum reflectors in its initial state (0 days) and after performing the SO<sub>2</sub> test for 21 days.

#### 4. Conclusions

This study proves that the presence of corrosive gases in the environment has an effect on the reflective layer of silvered glass reflectors when the pollutant is  $H_2S$ . The main signs of corrosion on the initially undamaged silvered reflective layer are found near the protected edges as micro spots (black spots smaller than 200  $\mu m$ ) as well as on the reflector surface as corrosion spots visible to the naked eye. As expected, the pre-damaged areas of the reflector (i.e., cut edges and scratch) are more deeply corroded.

Conversely, no significant signs of corrosion were observed in aluminum reflectors on performing accelerated corrosion tests with both sulfurous gases for 21 days. However, aluminum reflectors are also prone to corrosion according to other studies, especially in the presence of  $SO_2$  in acid rain conditions [25]. These results show prominent corrosion in this reflector type when the surrounding atmosphere is moist and the gas concentration is high. Therefore, both the concentration of the corrosive gas and its interaction with other factors, such as  $T$  and  $RH$ , must be considered when studying the durability of aluminum reflectors.

The results of this study show that silvered glass reflectors are suitable when a high optical performance is required and pollutant concentrations in the atmosphere are relatively low. Aluminum reflectors may be considered appropriate candidates if not very high specular values are needed in industrial environments, such as in small collectors for industrial process heat applications. Therefore, despite its lower reflectance, aluminum reflectors can be commercially competitive due to their simpler and more cost-efficient fabrication process, and their slower degradation rate in industrial environments, compared to silvered glass reflectors [25]. In past studies, aluminum degradation has been proven to be rather slow due to its protective  $SiO_2$  layer [22]. Studies also show that aluminum needs to be exposed to synergistic conditions (moisture, abrasion and pollutants) for a long time to be corroded [38].

Future research should focus on studying broader, more complex environmental conditions to reproduce the multiple possibilities of real outdoor exposure. For instance, a wider range of pollutant concentrations must be addressed to cover different polluted environments. Another prospective approach is the study of gas mixtures and the synergistic effects with the other factors in this multicomponent case. In addition, the results obtained in this study highlight the opportunity to study the durability of other CST components apart from reflectors, such as receivers, when they are subjected to corrosive sulfurous environments. It should be noted that comparisons of accelerated aging and real outdoor tests are being carried out to validate the durability studies of solar reflectors presented in this paper. These tests are being done in cooperation with plant operators and owners. However, these results have not been included, as outdoor testing campaigns have a medium- to long-term duration (at least 3–5 years).

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